

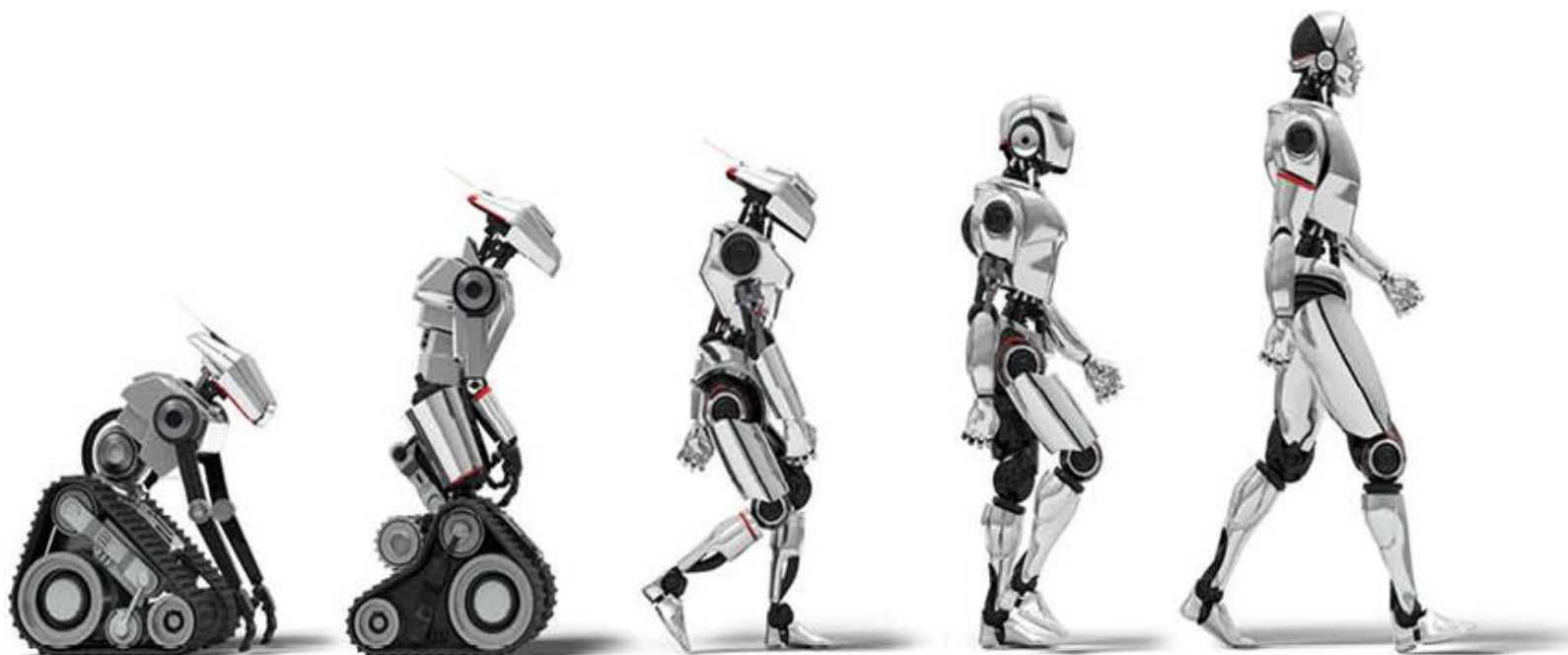


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Exercises Robotics 6



Geometric Jacobian Computation

In order to compute the Jacobian, it is convenient to proceed separately for the linear velocity and the angular velocity, this is called GEOMETRIC Jacobian.

For the contribution to the **linear velocity** of the end effector **e**, the time derivative of $\mathbf{p}_e(\mathbf{q})$ can be written as

$$\dot{\mathbf{p}}_e = \sum_{i=1}^n \frac{\partial \mathbf{p}_e}{\partial q_i} \dot{q}_i = \sum_{i=1}^n \mathbf{J}_{P_i} \dot{q}_i$$

NOTE:

Frame **0** and Frame **e** are taken as the base frame and the end-effector frame, respectively.

This expression shows how the velocity of \mathbf{p}_e can be obtained as the sum of the terms $\dot{q}_i \mathbf{j}_{P_i}$.

And we will use for this a sort of **superposition principle** considering each single joint contribution.

Jacobian Computation

$$\dot{\mathbf{p}}_e = \sum_{i=1}^n \frac{\partial \mathbf{p}_e}{\partial q_i} \dot{q}_i = \sum_{i=1}^n \mathbf{J}_{P_i} \dot{q}_i$$

Each term represents the contribution of the velocity of single **Joint i** to the end-effector linear velocity **when all the other joints are still.**

Therefore, by distinguishing the case of a *prismatic* joint ($q_i = d_i$) from the case of a *revolute* joint ($q_i = \vartheta_i$), it is:

$$\dot{q}_i \mathbf{J}_{P_i} = \dot{d}_i \mathbf{z}_{i-1}$$

If Joint i is *prismatic*, from

$$\mathbf{J}_{P_i} = \mathbf{z}_{i-1}.$$

$$\dot{q}_i \mathbf{J}_{P_i} = \boldsymbol{\omega}_{i-1,i} \times \mathbf{r}_{i-1,e} = \dot{\vartheta}_i \mathbf{z}_{i-1} \times (\mathbf{p}_e - \mathbf{p}_{i-1})$$

If Joint i is *revolute*

$$\mathbf{J}_{P_i} = \mathbf{z}_{i-1} \times (\mathbf{p}_e - \mathbf{p}_{i-1}).$$

Jacobian Computation

For the contribution to the **angular velocity**

$$\omega_e = \omega_n = \sum_{i=1}^n \omega_{i-1,i} = \sum_{i=1}^n \mathcal{J}_{O_i} \dot{q}_i,$$

Prismatic $\omega_{i-1,i} = \mathbf{0}$. $\mathbf{v}_{i-1,i} = \dot{d}_i \mathbf{z}_{i-1}$

Revolute $\omega_{i-1,i} = \dot{\vartheta}_i \mathbf{z}_{i-1}$,

Prismatic $\dot{q}_i \mathcal{J}_{O_i} = \mathbf{0}$ $\mathcal{J}_{O_i} = \mathbf{0}$.

Revolute $\dot{q}_i \mathcal{J}_{O_i} = \dot{\vartheta}_i \mathbf{z}_{i-1}$ $\mathcal{J}_{O_i} = \mathbf{z}_{i-1}$.

Jacobian Computation

$$\mathbf{v}_e = \begin{bmatrix} \dot{\mathbf{p}}_e \\ \boldsymbol{\omega}_e \end{bmatrix} = \mathbf{J}(\mathbf{q})\dot{\mathbf{q}} \quad \mathbf{J} = \begin{bmatrix} \mathcal{J}_{P1} & \cdots & \mathcal{J}_{Pn} \\ \mathcal{J}_{O1} & \cdots & \mathcal{J}_{On} \end{bmatrix},$$

$$\begin{bmatrix} \mathcal{J}_{Pi} \\ \mathcal{J}_{Oi} \end{bmatrix} = \begin{cases} \begin{bmatrix} \mathbf{z}_{i-1} \\ \mathbf{0} \end{bmatrix} & \text{for a } \textit{prismatic} \text{ joint} \\ \begin{bmatrix} \mathbf{z}_{i-1} \times (\mathbf{p}_e - \mathbf{p}_{i-1}) \\ \mathbf{z}_{i-1} \end{bmatrix} & \text{for a } \textit{revolute} \text{ joint.} \end{cases}$$

All the vectors \mathbf{z}_{i-1} , \mathbf{p}_e and \mathbf{p}_{i-1} are all functions of the joint variables.

Geometric Jacobian Computation

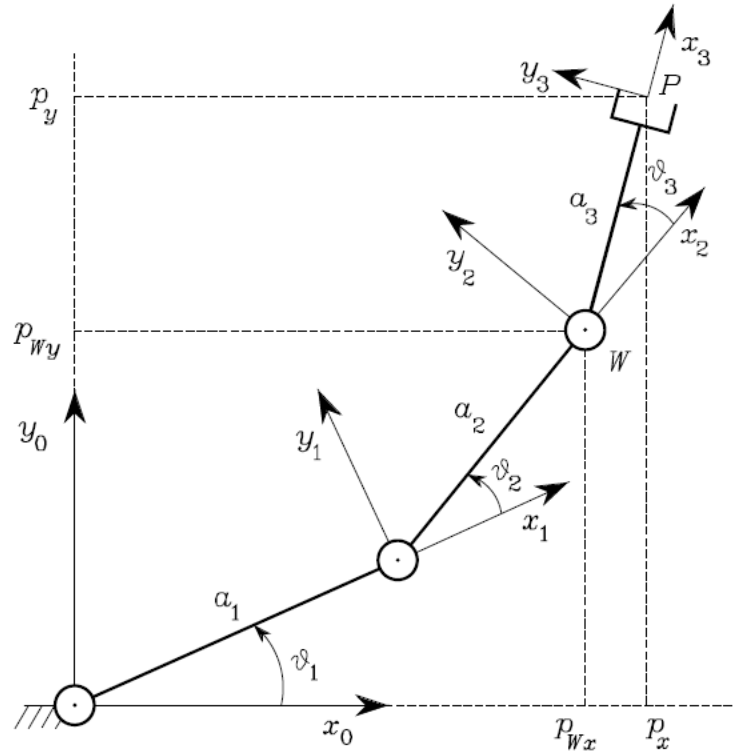
The Jacobian matrix depends on the frame in which the end-effector velocity is expressed.

The above equations allow computation of the geometric Jacobian with respect to the base frame. If it is desired to represent the Jacobian in a different Frame u , it is sufficient to know the relative rotation matrix R^u

$$\begin{bmatrix} \dot{p}_e^u \\ \omega_e^u \end{bmatrix} = \begin{bmatrix} R^u & O \\ O & R^u \end{bmatrix} \begin{bmatrix} \dot{p}_e \\ \omega_e \end{bmatrix}, \text{ which, substituted in } v_e = \begin{bmatrix} \dot{p}_e \\ \omega_e \end{bmatrix} = J(q)\dot{q}$$

$$\begin{bmatrix} \dot{p}_e^u \\ \omega_e^u \end{bmatrix} = \begin{bmatrix} R^u & O \\ O & R^u \end{bmatrix} J\dot{q} \quad J^u = \begin{bmatrix} R^u & O \\ O & R^u \end{bmatrix} J,$$

Geometric Jacobian: Three-link Planar Arm



$$T_3^0(\mathbf{q}) = A_1^0 A_2^1 A_3^2 = \begin{bmatrix} c_{123} & -s_{123} & 0 & a_1 c_1 + a_2 c_{12} + a_3 c_{123} \\ s_{123} & c_{123} & 0 & a_1 s_1 + a_2 s_{12} + a_3 s_{123} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

DH parameters for the three-link planar arm

| Link | a_i | α_i | d_i | ϑ_i |
|------|-------|------------|-------|---------------|
| 1 | a_1 | 0 | 0 | ϑ_1 |
| 2 | a_2 | 0 | 0 | ϑ_2 |
| 3 | a_3 | 0 | 0 | ϑ_3 |

Geometric Jacobian: Three-link Planar Arm

$$\begin{bmatrix} \mathbf{J}_{Pi} \\ \mathbf{J}_{Oi} \end{bmatrix} = \begin{cases} \begin{bmatrix} \mathbf{z}_{i-1} \\ \mathbf{0} \end{bmatrix} & \text{for a } \textit{prismatic} \text{ joint} \\ \begin{bmatrix} \mathbf{z}_{i-1} \times (\mathbf{p}_e - \mathbf{p}_{i-1}) \\ \mathbf{z}_{i-1} \end{bmatrix} & \text{for a } \textit{revolute} \text{ joint.} \end{cases}$$

$$\mathbf{J}(\mathbf{q}) = \begin{bmatrix} \mathbf{z}_0 \times (\mathbf{p}_3 - \mathbf{p}_0) & \mathbf{z}_1 \times (\mathbf{p}_3 - \mathbf{p}_1) & \mathbf{z}_2 \times (\mathbf{p}_3 - \mathbf{p}_2) \\ \mathbf{z}_0 & \mathbf{z}_1 & \mathbf{z}_2 \end{bmatrix}$$

Computation of the position vectors of the various links gives

$$\mathbf{p}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{p}_1 = \begin{bmatrix} a_1 c_1 \\ a_1 s_1 \\ 0 \end{bmatrix} \quad \mathbf{p}_2 = \begin{bmatrix} a_1 c_1 + a_2 c_{12} \\ a_1 s_1 + a_2 s_{12} \\ 0 \end{bmatrix} \quad \mathbf{p}_3 = \begin{bmatrix} a_1 c_1 + a_2 c_{12} + a_3 c_{123} \\ a_1 s_1 + a_2 s_{12} + a_3 s_{123} \\ 0 \end{bmatrix}$$

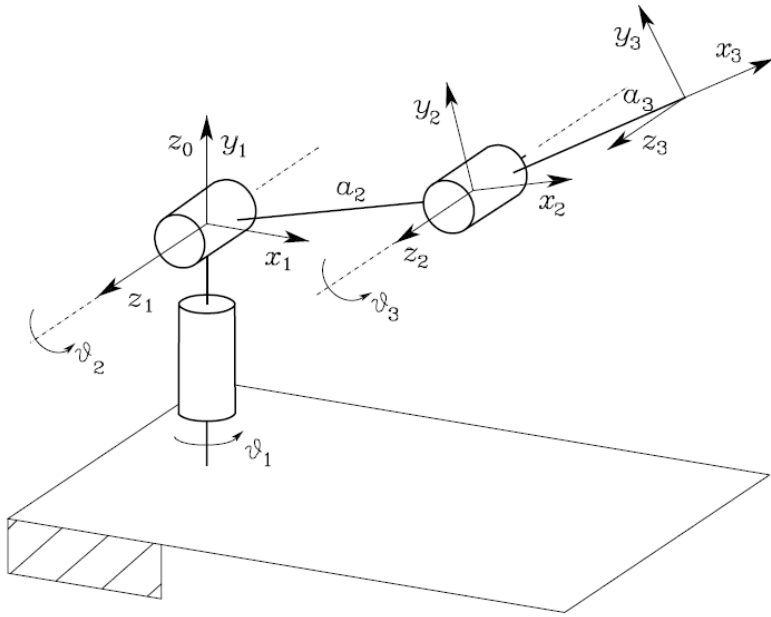
Geometric Jacobian: Three-link Planar Arm

$$\mathbf{p}_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{p}_1 = \begin{bmatrix} a_1 c_1 \\ a_1 s_1 \\ 0 \end{bmatrix} \quad \mathbf{p}_2 = \begin{bmatrix} a_1 c_1 + a_2 c_{12} \\ a_1 s_1 + a_2 s_{12} \\ 0 \end{bmatrix} \quad \mathbf{p}_3 = \begin{bmatrix} a_1 c_1 + a_2 c_{12} + a_3 c_{123} \\ a_1 s_1 + a_2 s_{12} + a_3 s_{123} \\ 0 \end{bmatrix}$$

while computation of the unit vectors of revolute joint axes gives since they are all parallel to **axis z₀**

$$\mathbf{z}_0 = \mathbf{z}_1 = \mathbf{z}_2 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \mathbf{J} = \begin{bmatrix} -a_1 s_1 - a_2 s_{12} - a_3 s_{123} & -a_2 s_{12} - a_3 s_{123} & -a_3 s_{123} \\ a_1 c_1 + a_2 c_{12} + a_3 c_{123} & a_2 c_{12} + a_3 c_{123} & a_3 c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$

Geometric Jacobian: Anthropomorphic Arm



| Link | a_i | α_i | d_i | ϑ_i |
|------|-------|------------|-------|---------------|
| 1 | 0 | $\pi/2$ | 0 | ϑ_1 |
| 2 | a_2 | 0 | 0 | ϑ_2 |
| 3 | a_3 | 0 | 0 | ϑ_3 |

$$\mathbf{A}_1^0(\vartheta_1) = \begin{bmatrix} c_1 & 0 & s_1 & 0 \\ s_1 & 0 & -c_1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{A}_i^{i-1}(\vartheta_i) = \begin{bmatrix} c_i & -s_i & 0 & a_i c_i \\ s_i & c_i & 0 & a_i s_i \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$i = 2, 3.$

$$\mathbf{T}_3^0(\mathbf{q}) = \mathbf{A}_1^0 \mathbf{A}_2^1 \mathbf{A}_3^2 = \begin{bmatrix} c_1 c_{23} & -c_1 s_{23} & s_1 & c_1 (a_2 c_2 + a_3 c_{23}) \\ s_1 c_{23} & -s_1 s_{23} & -c_1 & s_1 (a_2 c_2 + a_3 c_{23}) \\ s_{23} & c_{23} & 0 & a_2 s_2 + a_3 s_{23} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Geometric Jacobian: Anthropomorphic Arm

$$\mathbf{J} = \begin{bmatrix} \mathbf{z}_0 \times (\mathbf{p}_3 - \mathbf{p}_0) & \mathbf{z}_1 \times (\mathbf{p}_3 - \mathbf{p}_1) & \mathbf{z}_2 \times (\mathbf{p}_3 - \mathbf{p}_2) \\ \mathbf{z}_0 & \mathbf{z}_1 & \mathbf{z}_2 \end{bmatrix}$$

Computation of the position vectors of the various links gives

$$\mathbf{p}_0 = \mathbf{p}_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \quad \mathbf{p}_2 = \begin{bmatrix} a_2 c_1 c_2 \\ a_2 s_1 c_2 \\ a_2 s_2 \end{bmatrix} \quad \mathbf{p}_3 = \begin{bmatrix} c_1 (a_2 c_2 + a_3 c_{23}) \\ s_1 (a_2 c_2 + a_3 c_{23}) \\ a_2 s_2 + a_3 s_{23} \end{bmatrix}$$

computation of the unit vectors of revolute joint axes gives

$$\mathbf{z}_0 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \quad \mathbf{z}_1 = \mathbf{z}_2 = \begin{bmatrix} s_1 \\ -c_1 \\ 0 \end{bmatrix}.$$

Geometric Jacobian: Anthropomorphic Arm

$$\mathbf{J} = \begin{bmatrix} -s_1(a_2c_2 + a_3c_{23}) & -c_1(a_2s_2 + a_3s_{23}) & -a_3c_1s_{23} \\ c_1(a_2c_2 + a_3c_{23}) & -s_1(a_2s_2 + a_3s_{23}) & -a_3s_1s_{23} \\ 0 & a_2c_2 + a_3c_{23} & a_3c_{23} \\ 0 & s_1 & s_1 \\ 0 & -c_1 & -c_1 \\ 1 & 0 & 0 \end{bmatrix}$$

Having 3 DOFs only, it is worth considering the upper (3 × 3) block of the Jacobian

$$\mathbf{J}_P = \begin{bmatrix} -s_1(a_2c_2 + a_3c_{23}) & -c_1(a_2s_2 + a_3s_{23}) & -a_3c_1s_{23} \\ c_1(a_2c_2 + a_3c_{23}) & -s_1(a_2s_2 + a_3s_{23}) & -a_3s_1s_{23} \\ 0 & a_2c_2 + a_3c_{23} & a_3c_{23} \end{bmatrix} \quad \dot{\mathbf{p}}_e = \mathbf{J}_P(\mathbf{q})\dot{\mathbf{q}}$$

that describes the relationship between the joint velocities and the end-effector linear velocity.

Thank you for your Attention!!!

