

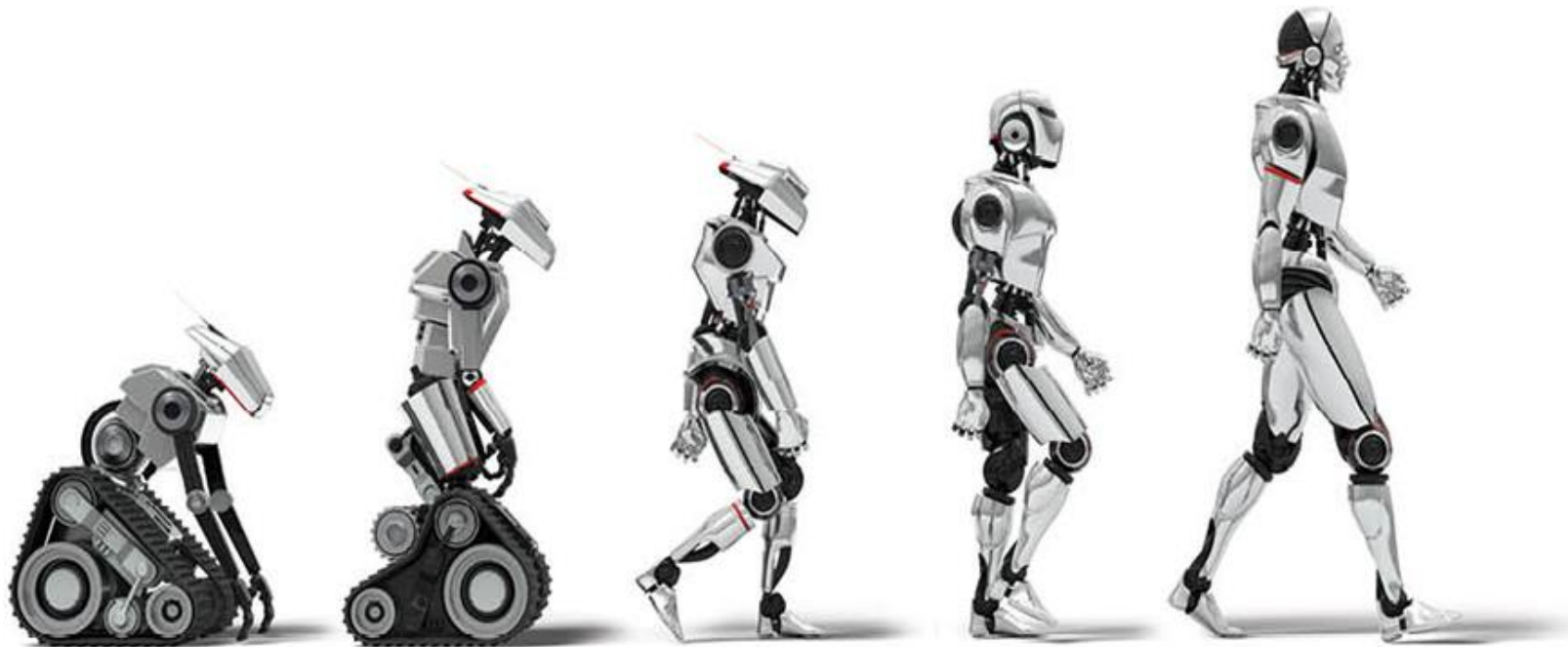


UNIVERSITÄT
HEIDELBERG
ZUKUNFT
SEIT 1386

Universität Heidelberg

Fakultät für Physik und Astronomie

Exercises Robotics 11



Jacobian

The kinematics of a 3R robot is defined by the following Denavit-Hartenberg table (units in [m] or [rad]):

i	α_i	a_i	d_i	θ_i
1	$\pi/2$	0	$d_1 = 5$	q_1
2	0	$a_2 = 4$	0	q_2
3	0	$a_3 = 3$	0	q_3

Determine the 3×3 linear part of the geometric Jacobian $\mathbf{J}(\mathbf{q})$ of this robot. When the robot is in the configuration $\mathbf{q}_0 = (\pi/2, \pi/4, \pi/2)$ [rad] and has a joint velocity $\dot{\mathbf{q}}_0 = (1, 2, -2)$ [rad/s], determine, if possible, a joint acceleration $\ddot{\mathbf{q}}$ that realizes a zero end-effector acceleration, i.e., $\ddot{\mathbf{p}} = \mathbf{0}$. [Bonus: What if the second link parameter is changed to $a_2 = 3$?]

Jacobian

The end-effector position is obtained from the homogenous transformation matrices:

$$\begin{aligned} \mathbf{p}_H &= \begin{pmatrix} \mathbf{p} \\ 1 \end{pmatrix} = {}^0\mathbf{A}_1(q_1) \left({}^1\mathbf{A}_2(q_2) \left({}^2\mathbf{A}_3(q_3) \begin{pmatrix} \mathbf{0} \\ 1 \end{pmatrix} \right) \right) \\ \implies \mathbf{p} = \mathbf{f}(\mathbf{q}) &= \begin{pmatrix} \cos q_1 (a_2 \cos q_2 + a_3 \cos(q_2 + q_3)) \\ \sin q_1 (a_2 \cos q_2 + a_3 \cos(q_2 + q_3)) \\ d_1 + a_2 \sin q_2 + a_3 \sin(q_2 + q_3) \end{pmatrix}. \end{aligned} \quad (1)$$

Therefore, using the usual compact notation for trigonometric functions, we have

$$\mathbf{J}(\mathbf{q}) = \frac{\partial \mathbf{f}(\mathbf{q})}{\partial \mathbf{q}} = \begin{pmatrix} -s_1 (a_2 c_2 + a_3 c_{23}) & -c_1 (a_2 s_2 + a_3 s_{23}) & -a_3 c_1 s_{23} \\ c_1 (a_2 c_2 + a_3 c_{23}) & -s_1 (a_2 s_2 + a_3 s_{23}) & -a_3 s_1 s_{23} \\ 0 & a_2 c_2 + a_3 c_{23} & a_3 c_{23} \end{pmatrix}. \quad (2)$$

The Jacobian is singular when¹

$$\det \mathbf{J}(\mathbf{q}) = -a_2 a_3 s_3 (a_2 c_2 + a_3 c_{23}) = 0. \quad (3)$$

Jacobian

The end-effector acceleration $\ddot{\mathbf{p}}$ is computed as

$$\ddot{\mathbf{p}} = \mathbf{J}(\mathbf{q})\ddot{\mathbf{q}} + \dot{\mathbf{J}}(\mathbf{q})\dot{\mathbf{q}}. \quad (4)$$

Thus, in order to realize a zero end-effector acceleration, we need to set $\ddot{\mathbf{p}} = \mathbf{0}$ in (4) and solve for $\ddot{\mathbf{q}}$, or

$$\ddot{\mathbf{q}} = -\mathbf{J}^{-1}(\mathbf{q})\dot{\mathbf{J}}(\mathbf{q})\dot{\mathbf{q}}. \quad (5)$$

Indeed, this solution is valid as long as the robot is out of singularities. To evaluate (5), we need first to derive the time derivative of the robot Jacobian. Let $\mathbf{J}_i(\mathbf{q})$ be the i th column of the Jacobian $\mathbf{J}(\mathbf{q})$, for $i = 1, 2, 3$. We compute

$$\begin{aligned} \dot{\mathbf{J}}(\mathbf{q}) &= \frac{d\mathbf{J}(\mathbf{q})}{dt} \left(= \sum_{i=1}^3 \frac{\partial \mathbf{J}_i(\mathbf{q})}{\partial \mathbf{q}} \dot{\mathbf{q}} = \sum_{j=1}^3 \frac{\partial \mathbf{J}(\mathbf{q})}{\partial q_j} \dot{q}_j \right) \\ &= \begin{pmatrix} -c_1 \dot{q}_1 (a_2 c_2 + a_3 c_{23}) + s_1 (a_2 s_2 \dot{q}_2 + a_3 s_{23} (\dot{q}_2 + \dot{q}_3)) \\ -s_1 \dot{q}_1 (a_2 c_2 + a_3 c_{23}) - c_1 (a_2 s_2 \dot{q}_2 + a_3 s_{23} (\dot{q}_2 + \dot{q}_3)) \\ 0 \\ s_1 \dot{q}_1 (a_2 s_2 + a_3 s_{23}) - c_1 (a_2 c_2 \dot{q}_2 + a_3 c_{23} (\dot{q}_2 + \dot{q}_3)) & a_3 s_1 \dot{q}_1 s_{23} - a_3 c_1 c_{23} (\dot{q}_2 + \dot{q}_3) \\ c_1 \dot{q}_1 (a_2 s_2 + a_3 s_{23}) - s_1 (a_2 c_2 \dot{q}_2 + a_3 c_{23} (\dot{q}_2 + \dot{q}_3)) & -a_3 c_1 \dot{q}_1 s_{23} - a_3 s_1 c_{23} (\dot{q}_2 + \dot{q}_3) \\ -(a_2 s_2 \dot{q}_2 - a_3 s_{23} (\dot{q}_2 + \dot{q}_3)) & -a_3 s_{23} (\dot{q}_2 + \dot{q}_3) \end{pmatrix}. \end{aligned} \quad (6)$$

Jacobian

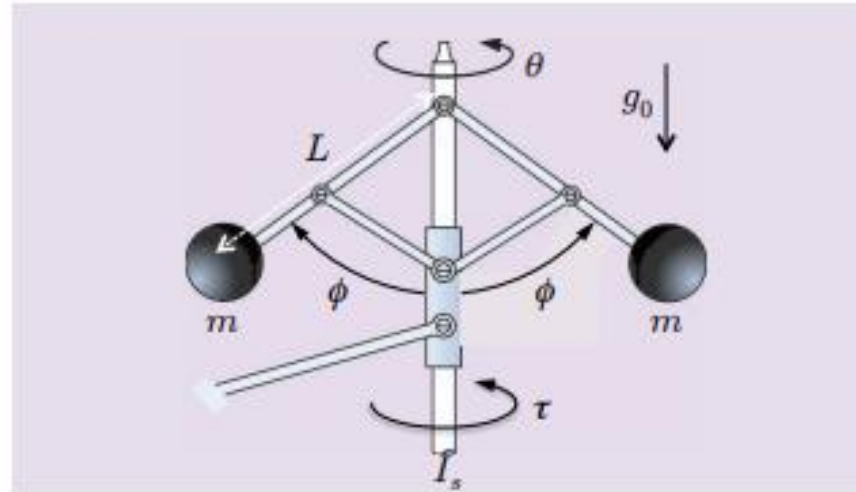
When the robot is in the configuration $\mathbf{q}_0 = (\pi/2, \pi/4, \pi/2)$ [rad] and has a joint velocity $\dot{\mathbf{q}}_0 = (1, 2, -2)$ [rad/s], evaluation of (2) and (6) gives

$$\mathbf{J}_0 = \mathbf{J}(\mathbf{q}_0) = \begin{pmatrix} -0.7071 & 0 & 0 \\ 0 & -4.9497 & -2.1213 \\ 0 & 0.7071 & -2.1213 \end{pmatrix}, \quad \dot{\mathbf{J}}_0 = \dot{\mathbf{J}}(\mathbf{q}_0)|_{\dot{\mathbf{q}}=\dot{\mathbf{q}}_0} = \begin{pmatrix} 5.6569 & 4.9497 & 2.1213 \\ -0.7071 & -5.6569 & 0 \\ 0 & -5.6569 & 0 \end{pmatrix}.$$

Since $\det \mathbf{J}_0 = -8.4853 \neq 0$, we can use eq. (5) for computing the joint acceleration $\ddot{\mathbf{q}}$ that realizes a zero end-effector acceleration:

$$\ddot{\mathbf{q}} = -\mathbf{J}_0^{-1} (\dot{\mathbf{J}}_0 \dot{\mathbf{q}}_0) = - \begin{pmatrix} -1.4142 & 0 & 0 \\ 0 & -0.1768 & 0.1768 \\ 0 & -0.0589 & -0.4125 \end{pmatrix} \begin{pmatrix} 11.3137 \\ -12.0208 \\ -11.3137 \end{pmatrix} = \begin{pmatrix} 16 \\ -0.1250 \\ -5.3750 \end{pmatrix} \text{ [rad/s}^2\text{]}. \quad (7)$$

Lagrangian



Assume that:

- the main shaft has an inertia I_s around its rotation axis
- the two balls have identical mass m that is concentrated at the end of a link of length L
- the links and all other linkages have negligible masses
- a viscous friction torque with coefficient $f_v > 0$ is acting on the main shaft
- all other frictional effects are negligible.

Derive the complete dynamic model of this system using a Lagrangian formalism. Assuming knowledge of the geometric parameter L , provide a linear parametrization of the dynamics in terms of its dynamic coefficients.

Thank you for your Attention!!!

